



# Enhancement microwave dielectric properties of $\text{La}(\text{Mg}_{0.5}\text{Sn}_{0.5})\text{O}_3$ ceramics by substituting $\text{Mg}^{2+}$ with $\text{Ni}^{2+}$

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## ABSTRACT

The microwave dielectric properties of  $\text{La}(\text{Mg}_{0.5-x}\text{Ni}_x\text{Sn}_{0.5})\text{O}_3$  ceramics were examined with a view to their exploitation for mobile communication. The  $\text{La}(\text{Mg}_{0.5-x}\text{Ni}_x\text{Sn}_{0.5})\text{O}_3$  ceramics were prepared by the conventional solid-state method at various sintering temperatures. The X-ray diffraction patterns of the  $\text{La}(\text{Mg}_{0.4}\text{Ni}_{0.1}\text{Sn}_{0.5})\text{O}_3$  ceramics revealed no significant variation of phase with sintering temperatures. Apparent density of  $6.71 \text{ g/cm}^3$ , dielectric constant ( $\epsilon_r$ ) of 20.19, quality factor ( $Q \times f$ ) of 74,600 GHz, and temperature coefficient of resonant frequency ( $\tau_f$ ) of  $-85 \text{ ppm/}^\circ\text{C}$  were obtained for  $\text{La}(\text{Mg}_{0.4}\text{Ni}_{0.1}\text{Sn}_{0.5})\text{O}_3$  ceramics that were sintered at  $1550^\circ\text{C}$  for 4 h.

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## 1. Introduction

The advantages provided by using complex perovskite ceramics  $\text{A}(\text{B}'_{0.5}\text{B}''_{0.5})\text{O}_3$  ( $\text{A} = \text{Me}^{2+}, \text{Me}^{3+}$ ;  $\text{B}' = \text{Me}^{2+}, \text{Me}^{3+}$ ;  $\text{B}'' = \text{Me}^{4+}, \text{Me}^{5+}, \text{Me}^{6+}$ ) are reportedly associated with their excellent dielectric properties at microwave frequencies. A dielectric constant of 19.3 and a  $Q \times f$  of 43,300 GHz were obtained when  $\text{Nd}(\text{Mg}_{0.5}\text{Sn}_{0.5})\text{O}_3$  ceramics were sintered at  $1550^\circ\text{C}$  for 4 h [1]. A dielectric constant of 15.6 and a  $Q \times f$  of 30,600 GHz were obtained for  $\text{La}(\text{Mg}_{0.5}\text{Sn}_{0.5})\text{O}_3$  ceramics that were sintered at  $1500^\circ\text{C}$  for 4 h [2]. A liquid phase flux such as  $\text{CuO}$  and  $\text{B}_2\text{O}_3$  was added to improve the microwave dielectric properties of  $\text{La}(\text{Mg}_{0.5}\text{Sn}_{0.5})\text{O}_3$  ceramics. A dielectric constant of 19.7 and a  $Q \times f$  of 43,300 GHz were obtained for  $\text{La}(\text{Mg}_{0.5}\text{Sn}_{0.5})\text{O}_3$  ceramics with 0.5 wt%  $\text{CuO}$  additive that were sintered at  $1550^\circ\text{C}$  for 4 h [3].  $\text{La}(\text{Mg}_{0.5}\text{Sn}_{0.5})\text{O}_3$  ceramics with 0.5 wt%  $\text{B}_2\text{O}_3$  additive, sintered at  $1500^\circ\text{C}$  for 4 h, have been obtained with a dielectric constant of 19.7 and a  $Q \times f$  of 45,000 GHz [4].  $\text{La}_{2.98/3}\text{Ba}_{0.01}(\text{Mg}_{0.5}\text{Sn}_{0.5})\text{O}_3$  have been synthesized with  $\text{La}^{3+}$  ions substituted partially with  $\text{Ba}^{2+}$  ions to improve the microwave dielectric properties. A dielectric constant of 19.8, and a  $Q \times f$  of 46,500 GHz were obtained for  $\text{La}_{2.98/3}\text{Ba}_{0.01}(\text{Mg}_{0.5}\text{Sn}_{0.5})\text{O}_3$  ceramics with 0.25 wt%  $\text{B}_2\text{O}_3$  additive sintered at  $1400^\circ\text{C}$  for 4 h [5]. Since the ionic radius of  $\text{Bi}^{3+}$  (0.103 nm) is similar to that of  $\text{La}^{3+}$

(0.1032 nm), the  $\text{La}^{3+}$  ion can be substituted by the  $\text{Bi}^{3+}$  ion to form  $\text{La}_{1-x}\text{Bi}_x(\text{Mg}_{0.5}\text{Sn}_{0.5})\text{O}_3$  ceramics. A dielectric constant of 20.2 and a  $Q \times f$  of 58,100 GHz were obtained for  $\text{La}_{0.97}\text{Bi}_{0.03}(\text{Mg}_{0.5}\text{Sn}_{0.5})\text{O}_3$  ceramics that were sintered at  $1550^\circ\text{C}$  for 4 h [6]. Combining two compounds with negative and positive temperature coefficients of resonant frequency is effective approach to obtain a near zero temperature coefficient of resonant frequency.  $0.4\text{La}(\text{Mg}_{1/2}\text{Ti}_{1/2})\text{O}_3-0.6(\text{Na}_{0.5}\text{Nd}_{0.5})\text{TiO}_3$  ceramics with 1 wt%  $\text{B}_2\text{O}_3$  addition possesses a dielectric constant of 42, a  $Q \times f$  of 33,000 GHz and a temperature coefficient of resonant frequency of  $0.5 \text{ ppm/}^\circ\text{C}$  that were sintered at  $1475^\circ\text{C}$  [7].  $0.55\text{La}(\text{Mg}_{1/2}\text{Ti}_{1/2})\text{O}_3-0.45\text{SrTiO}_3$  ceramics with 0.25%  $\text{B}_2\text{O}_3$  sintered at  $1475^\circ\text{C}$  for 4 h in air exhibited optimum microwave dielectric properties of dielectric constant of 46.32, a  $Q \times f$  of 34,000 GHz and a temperature coefficient of resonant frequency of  $-0.12 \text{ ppm/}^\circ\text{C}$  [8]. At  $1425^\circ\text{C}$ ,  $0.87\text{La}(\text{Mg}_{1/2}\text{Ti}_{1/2})\text{O}_3-0.13\text{Ca}_{0.8}\text{Sr}_{0.2}\text{TiO}_3$  ceramics with 0.5 wt%  $\text{B}_2\text{O}_3$  addition possesses a dielectric constant of 38.3, a  $Q \times f$  value of 59,800 GHz and a temperature coefficients of resonant frequency of  $0 \text{ ppm/}^\circ\text{C}$  [9].  $0.4\text{La}(\text{Mg}_{1/2}\text{Ti}_{1/2})\text{O}_3-0.6(\text{Na}_{0.5}\text{Nd}_{0.5})\text{TiO}_3$  ceramics with 1 wt%  $\text{B}_2\text{O}_3$  addition possesses a dielectric constant of 42, a  $Q \times f$  of 33,000 GHz and a temperature coefficient of resonant frequency of  $0.5 \text{ ppm/}^\circ\text{C}$  that were sintered at  $1475^\circ\text{C}$  [7]. At  $1475^\circ\text{C}$ ,  $0.6\text{La}(\text{Mg}_{1/2}\text{Ti}_{1/2})\text{O}_3-0.4\text{Ca}_{0.6}\text{Nd}_{0.8/3}\text{TiO}_3$  ceramics with 0.5 wt%  $\text{B}_2\text{O}_3$  addition possesses a dielectric constant of 39, a  $Q \times f$  of 41,000 GHz and a temperature coefficient of resonant frequency of  $-2.6 \text{ ppm/}^\circ\text{C}$  [10]. The optimum combination of microwave dielectric properties was achieved at  $1475^\circ\text{C}$  for samples where  $0.5\text{La}(\text{Mg}_{0.5}\text{Ti}_{0.5})\text{O}_3-0.5(\text{Ca}_{0.8}\text{Sr}_{0.2})\text{TiO}_3$

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with a dielectric constant of 47.12, a  $Q \times f$  value of 35,000 GHz and a temperature coefficient of resonant frequency value of  $-4.7 \text{ ppm}/^\circ\text{C}$  [11]. A new microwave dielectric material  $0.45\text{La}(\text{Mg}_{0.5}\text{Ti}_{0.5})\text{O}_3-0.55\text{Ca}_{0.8}\text{Sm}_{0.4/3}\text{TiO}_3$ , possessing a fine combination of microwave dielectric properties with a dielectric constant of 47.83, a  $Q \times f$  of 26,500 GHz and a temperature coefficient of resonant frequency of  $-1.7 \text{ ppm}/^\circ\text{C}$  [12].  $0.6\text{La}(\text{Mg}_{1/2}\text{Ti}_{1/2})\text{O}_3-0.4(\text{La}_{0.5}\text{Na}_{0.5})\text{TiO}_3$  ceramics with 1 wt%  $\text{B}_2\text{O}_3$  addition possesses a dielectric constant of 36, a  $Q \times f$  value of 25,500 GHz and a temperature coefficients of resonant frequency of  $-5 \text{ ppm}/^\circ\text{C}$  sintering at  $1475^\circ\text{C}$  [13]. A dielectric constant of 37, a  $Q \times f$  value of 34,100 GHz and a temperature coefficient of resonant of  $13.5 \text{ ppm}/^\circ\text{C}$  were obtained for  $0.1\text{CaTiO}_3-0.9\text{Nd}(\text{Mg}_{1/2}\text{Ti}_{1/2})\text{O}_3$  ceramics that sintered at  $1325^\circ\text{C}$  for 4 h [14]. At  $1375^\circ\text{C}$ ,  $0.4\text{Nd}(\text{Mg}_{1/2}\text{Ti}_{1/2})\text{O}_3-0.6\text{Ca}_{0.6}\text{La}_{0.8/3}\text{TiO}_3$  ceramics with 1 wt%  $\text{B}_2\text{O}_3$  addition possesses a dielectric constant of 49, a  $Q \times f$  value of 13,000 GHz and a temperature coefficients of resonant frequency of  $1 \text{ ppm}/^\circ\text{C}$  [15]. At  $1475^\circ\text{C}$ ,  $0.1\text{SrTiO}_3-0.9\text{Nd}(\text{Mg}_{1/2}\text{Ti}_{1/2})\text{O}_3$  has a dielectric constant of 45.4, a  $Q \times f$  value of 44,000 GHz and a temperature coefficient of resonant frequency of  $-3 \text{ ppm}/^\circ\text{C}$  [16].

Since the ionic radius of  $\text{Ni}^{2+}$  (0.069 nm) is similar to that of  $\text{Mg}^{2+}$  (0.072 nm), the  $\text{Mg}^{2+}$  ion can be replaced by with the  $\text{Ni}^{2+}$  ion to form  $\text{La}(\text{Mg}_{0.5-x}\text{Ni}_x\text{Sn}_{0.5})\text{O}_3$  [17]. In this investigation,  $\text{La}(\text{Mg}_{0.5-x}\text{Ni}_x\text{Sn}_{0.5})\text{O}_3$  were synthesized and some of the  $\text{Mg}^{2+}$  ions were substituted with  $\text{Ni}^{2+}$  ions to improve their microwave dielectric properties. Moreover, the effect of the sintering temperature on the microwave dielectric properties of  $\text{La}(\text{Mg}_{0.5-x}\text{Ni}_x\text{Sn}_{0.5})\text{O}_3$  ceramics was studied.  $\text{La}(\text{Mg}_{0.5-x}\text{Ni}_x\text{Sn}_{0.5})\text{O}_3$  ceramics were synthesized by the conventional mixed-oxide method and demonstrated to have better microwave dielectric properties than  $\text{La}(\text{Mg}_{0.5}\text{Sn}_{0.5})\text{O}_3$  ceramics. The microwave dielectric properties of  $\text{La}(\text{Mg}_{0.5-x}\text{Ni}_x\text{Sn}_{0.5})\text{O}_3$  ceramics were found to vary with the degree of  $\text{Ni}^{2+}$  substitution and sintering temperatures. These various microwave dielectric properties were analyzed by densification, X-ray diffraction (XRD) patterns, and observation of their microstructures.

## 2. Experimental procedures

The starting raw chemicals were  $\text{La}_2\text{O}_3$  (99.99%),  $\text{MgO}$  (98.0%),  $\text{NiO}$  (99.97%), and  $\text{SnO}_2$  (99.0%) powder. The prepared composition was  $\text{La}(\text{Mg}_{0.5-x}\text{Ni}_x\text{Sn}_{0.5})\text{O}_3$ . Specimens were prepared using the conventional mixed-oxide method. The raw material was weighed out in stoichiometric proportions after drying  $\text{La}_2\text{O}_3$  at  $1000^\circ\text{C}$  for 4 h to remove moisture content. The raw material was ball-milled in alcohol for 12 h, dried, and then calcined at  $1200^\circ\text{C}$  for 4 h. The calcined powder was re-milled for 12 h using PVA solution as a binder. The obtained fine powder was then crushed into a finer powder through a sieve with a 200 mesh. This finer powder was then axially pressed at  $2000 \text{ kg}/\text{cm}^2$  into pellets with a diameter of 11 mm and a thickness of 6 mm. The specimens thus obtained were then sintered at temperatures of  $1450$ – $1600^\circ\text{C}$  for 4 h in air. Both the heating rate and the cooling rate were set to  $10^\circ\text{C}/\text{min}$ .

After sintering, the phases of the samples were investigated by X-ray diffraction. An X-ray Rigaku D/MAX-2200 was used with  $\text{CuK}\alpha$  radiation (at 30 kV and 20 mA) and a graphite monochromator in the  $2\theta$  range of  $20^\circ$ – $80^\circ$ . Scanning electron microscopy (SEM; JEOL JSM-6500F) and energy dispersive X-ray spectrometer (EDS) were utilized to examine the microstructures of the specimens. The apparent densities of the specimens were measured by the liquid Archimedes method using distilled water. The microwave dielectric properties of the specimens were measured by the postresonator method that was developed by Hakki and Coleman [18]. This method employs a specimen in the form of a cylinder of diameter  $D$  and length  $L$ . The specimens used for making microwave dielectric property measurements had an aspect ratio  $D/L$  of about 1.6, which is in the permitted range that was determined by Kobayashi and Katoh [19]. The cylindrical resonator was sandwiched between two conducting plates. Two small antennas were positioned in the vicinity of the specimen to couple the microwave signal power into or out of the resonator. The other ends of the antennas were connected to an Agilent E5071C network analyzer. The resonance characteristics depended on the size and the microwave dielectric properties of the specimen. The microwave energy was coupled using electric-field probes. The  $\text{TE}_{011}$  resonant mode was optimal for obtaining the dielectric constant and the loss factor of the specimen. The Agilent E5071C network analyzer was used to identify the  $\text{TE}_{011}$  resonant frequency of the dielectric resonator, and the dielectric constant and quality factor were calculated. The technique for measuring  $\tau_f$  was the

same as that for measuring the dielectric constant. The test cavity was placed in a chamber and the temperature was increased from  $25$  to  $75^\circ\text{C}$ . The  $\tau_f$  value ( $\text{ppm}/^\circ\text{C}$ ) was determined from the change in resonant frequency:  $(1)\tau_f = \frac{f_2 - f_1}{f_1(T_2 - T_1)}$ , where  $f_1$  and  $f_2$  represent the resonant frequencies at  $T_1$  and  $T_2$ , respectively.

## 3. Results and discussion

Fig. 1 shows the X-ray diffraction patterns of  $\text{La}(\text{Mg}_{0.4}\text{Ni}_{0.1}\text{Sn}_{0.5})\text{O}_3$  ceramics that were sintered at  $1450$ – $1600^\circ\text{C}$  for 4 h. Clearly,  $\text{La}(\text{Mg}_{0.4}\text{Ni}_{0.1}\text{Sn}_{0.5})\text{O}_3$  is the main crystalline phase, which is accompanied by small amounts of  $\text{La}_2\text{Sn}_2\text{O}_7$  as the second phase. The formation of  $\text{La}_2\text{Sn}_2\text{O}_7$  might deteriorate the dielectric constant and quality factor of the specimen. A later investigation will involve preparation of the powder by precipitation from solution. Such a method may yield a single-phase product. A single-phase product potentially has much higher values of the parameters of interest. All of the peaks were indexed based on the cubic perovskite unit cell. A series of extra peaks were observed to correspond to superlattice reflections. All of the superlattice reflections were indexed using half-integer Miller indices. According to Glazer, the superlattice reflections, with specific combinations of odd (o) and even (e) Miller indices, reveal particular deviations of the structure from the undistorted cubic structure, such as octahedral in-phase tilting (ooo, oeo, eoo), anti-phase tilting (ooo,  $h+k+l>3$ ), and anti-parallel displacement of A-cations (eoe, eoe, oee) [20]. The  $(1/2(210), 1/2(300), 1/2(320), 1/2(410), 1/2(421), 1/2(432)$  and  $1/2(441))$  extra peaks indicate A-site cation displacement, the  $(1/2(311), 1/2(331), 1/2(511)$  and  $1/2(531))$  peaks reveal anti-phase tilting, and the  $1/2(321)$  peak show in-phase tilting. The X-ray diffraction patterns of  $\text{La}(\text{Mg}_{0.4}\text{Ni}_{0.1}\text{Sn}_{0.5})\text{O}_3$  ceramics did not significantly vary with sintering temperature. Fig. 2 shows the X-ray diffraction patterns of  $\text{La}(\text{Mg}_{0.5-x}\text{Ni}_x\text{Sn}_{0.5})\text{O}_3$  ceramics as  $x$  is varied from 0 to 0.15, following sintering at  $1550^\circ\text{C}$  for 4 h. The diffraction peaks of  $\text{La}(\text{Mg}_{0.5-x}\text{Ni}_x\text{Sn}_{0.5})\text{O}_3$  ceramics shifted to higher angles as  $x$  increased, perhaps because the ionic

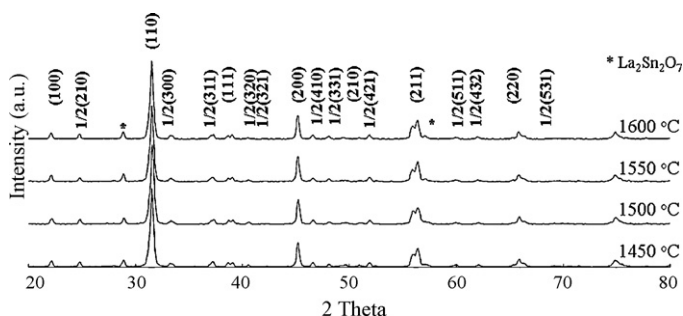


Fig. 1. X-ray diffraction patterns of  $\text{La}(\text{Mg}_{0.4}\text{Ni}_{0.1}\text{Sn}_{0.5})\text{O}_3$  specimens sintered at  $1450$ – $1600^\circ\text{C}$  for 4 h (\*:  $\text{La}_2\text{Sn}_2\text{O}_7$ ).

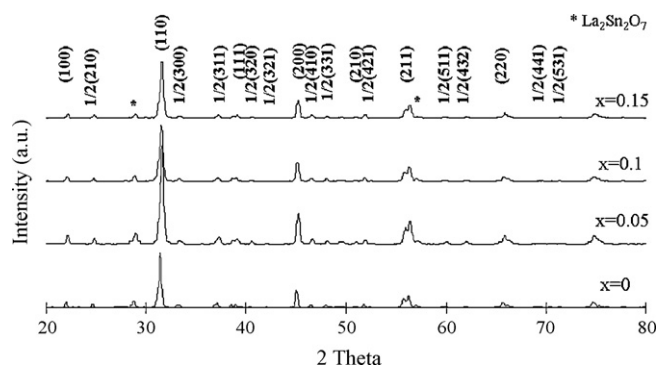


Fig. 2. X-ray diffraction patterns of  $\text{La}(\text{Mg}_{0.5-x}\text{Ni}_x\text{Sn}_{0.5})\text{O}_3$  ceramics that were sintered at  $1550^\circ\text{C}$  for 4 h (\*:  $\text{La}_2\text{Sn}_2\text{O}_7$ ).

**Table 1**  
Amount of main phase, grain size and  $Q \times f$  of  $\text{La}(\text{Mg}_{0.5-x}\text{Ni}_x\text{Sn}_{0.5})\text{O}_3$  ceramics following sintering at  $1550^\circ\text{C}$  for 4 h.

Material	Main phase (%)	Grain size ( $\mu\text{m}$ )	$Q \times f$ (GHz)
$\text{La}(\text{Mg}_{0.5}\text{Sn}_{0.5})\text{O}_3$	89.09	0.85	45,900
$\text{La}(\text{Mg}_{0.45}\text{Ni}_{0.05}\text{Sn}_{0.5})\text{O}_3$	89.77	1.49	64,400
$\text{La}(\text{Mg}_{0.4}\text{Ni}_{0.1}\text{Sn}_{0.5})\text{O}_3$	90.14	1.43	74,600
$\text{La}(\text{Mg}_{0.35}\text{Ni}_{0.15}\text{Sn}_{0.5})\text{O}_3$	91.98	1.29	39,000

radius of  $\text{Ni}^{2+}$  ions (0.069 nm) is smaller than that of  $\text{Mg}^{2+}$  ions (0.072 nm). The amount of main phase was evaluated from most intensive lines of main and second phases,

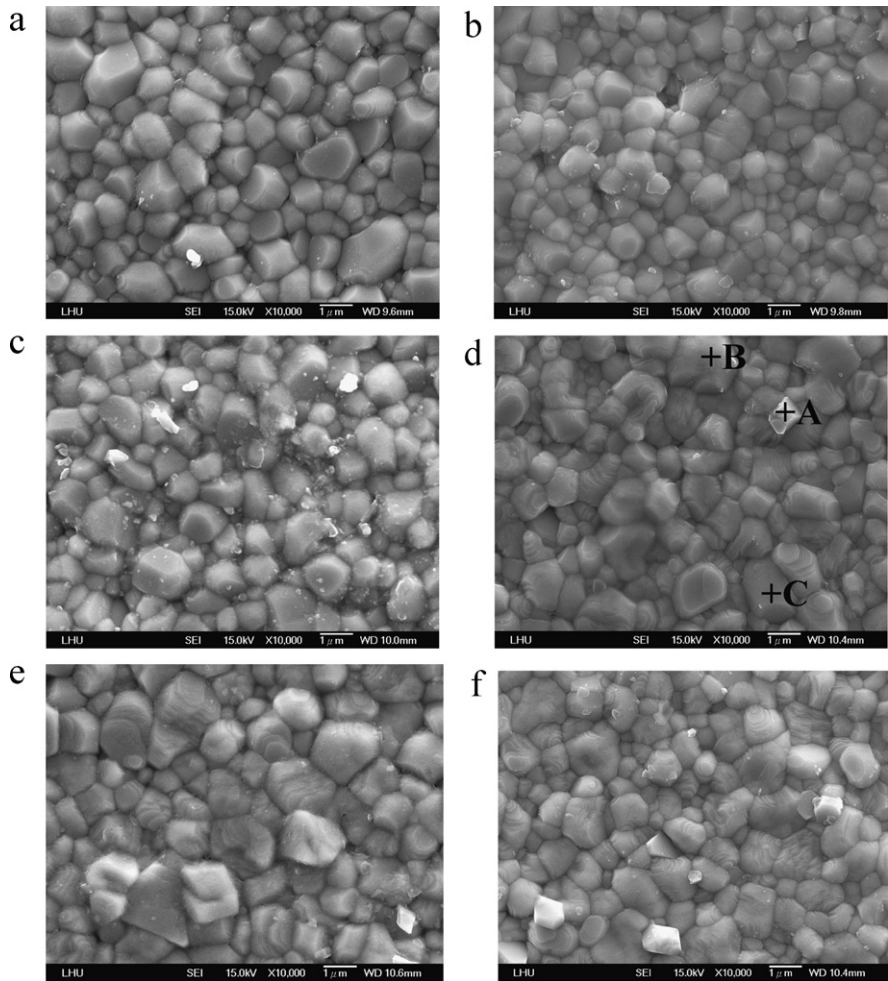
$$\text{Main phase (\%)} = \frac{I_{\text{main}}}{I_{\text{main}} + I_{\text{second}}} \times 100, \quad (2)$$

where  $I_{\text{main}}$  is the most intensive line of main phase and  $I_{\text{second}}$  is the most intensive line of second phase. Table 1 shows the amount of main phase of  $\text{La}(\text{Mg}_{0.5-x}\text{Ni}_x\text{Sn}_{0.5})\text{O}_3$  ceramics that were sintered at  $1550^\circ\text{C}$  for 4 h. The amount of main phase increased from 89.09% to 91.98% as  $x$  increased from 0 to 0.15. The tolerance factors of  $\text{La}(\text{Mg}_{0.5-x}\text{Ni}_x\text{Sn}_{0.5})\text{O}_3$  ceramics increased from 0.914 to 0.916 as  $x$  increased from 0 to 0.15. The tolerance factors were calculated using the ionic radius data of Shannon [17]. The tolerance factors of  $\text{La}(\text{Mg}_{0.5-x}\text{Ni}_x\text{Sn}_{0.5})\text{O}_3$  series are in the anti-phase and in-phase titled region [21], which is in agreement with those of X-ray diffraction patterns as describe above.

**Table 2**  
EDS data of grains of  $\text{La}(\text{Mg}_{0.4}\text{Ni}_{0.1}\text{Sn}_{0.5})\text{O}_3$  ceramics sintered at  $1550^\circ\text{C}$  for 4 h.

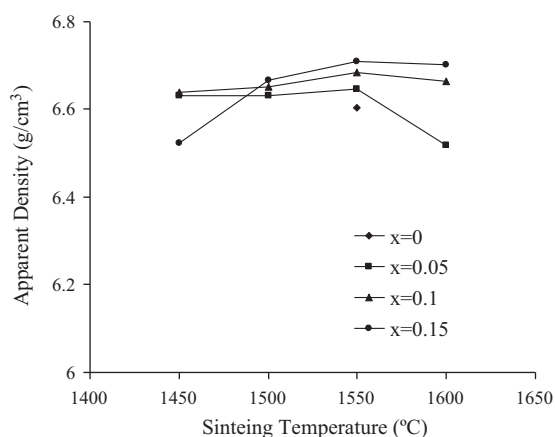
Atomic element	La (%)	Mg (%)	Ni (%)	Sn (%)	O (%)
A	17.48	0.00	0.00	16.33	66.19
B	17.05	7.48	0.86	8.27	66.35
C	14.27	6.54	1.28	6.85	71.05

Fig. 3 shows the microstructures of  $\text{La}(\text{Mg}_{0.5-x}\text{Ni}_x\text{Sn}_{0.5})\text{O}_3$  ceramics following sintering for 4 h at different temperatures. The microstructures of  $\text{La}(\text{Mg}_{0.5-x}\text{Ni}_x\text{Sn}_{0.5})\text{O}_3$  ceramics when  $\text{Mg}^{2+}$  ions were replaced with different degrees of  $\text{Ni}^{2+}$  ions indicated that the average grain size did not vary significantly with  $x$  varied from 0.05 to 0.10. The average grain size decreased from 1.43 to  $1.29 \mu\text{m}$  as  $x$  increased from 0.1 to 0.15. Comparing the microstructures of  $\text{La}(\text{Mg}_{0.4}\text{Ni}_{0.1}\text{Sn}_{0.5})\text{O}_3$  ceramics that were sintered under different temperatures indicated that the average grain size increased from  $1.16$  to  $1.64 \mu\text{m}$  as sintering temperature increased from  $1450$  to  $1600^\circ\text{C}$ . The pores of  $\text{La}(\text{Mg}_{0.4}\text{Ni}_{0.1}\text{Sn}_{0.5})\text{O}_3$  ceramics almost disappeared upon sintering at  $1550^\circ\text{C}$  for 4 h. To identify the composition of the second phase, energy-disperse spectroscopy (EDS) analysis was carried out on the grains of  $\text{La}(\text{Mg}_{0.4}\text{Ni}_{0.1}\text{Sn}_{0.5})\text{O}_3$  ceramics that were sintered at  $1550^\circ\text{C}$  for 4 h, as shown in Fig. 3(d). According to the quantitative analysis, as shown in Table 2, the A grain is  $\text{La}_2\text{Sn}_2\text{O}_7$  and the B and C grains are  $\text{La}(\text{Mg}_{0.4}\text{Ni}_{0.1}\text{Sn}_{0.5})\text{O}_3$ .



**Fig. 3.** Microstructures of  $\text{La}(\text{Mg}_{0.5-x}\text{Ni}_x\text{Sn}_{0.5})\text{O}_3$  ceramics sintered under different temperatures for 4 h: (a)  $x=0.05/1550^\circ\text{C}$ , (b)  $x=0.1/1450^\circ\text{C}$ , (c)  $x=0.1/1500^\circ\text{C}$ , (d)  $x=0.1/1550^\circ\text{C}$ , (e)  $x=0.1/1600^\circ\text{C}$ , and (f)  $x=0.15/1550^\circ\text{C}$ .

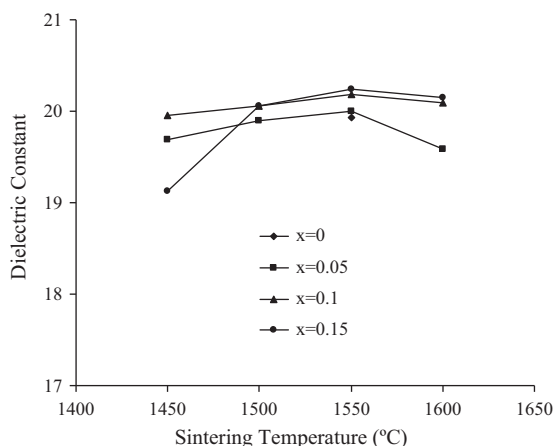




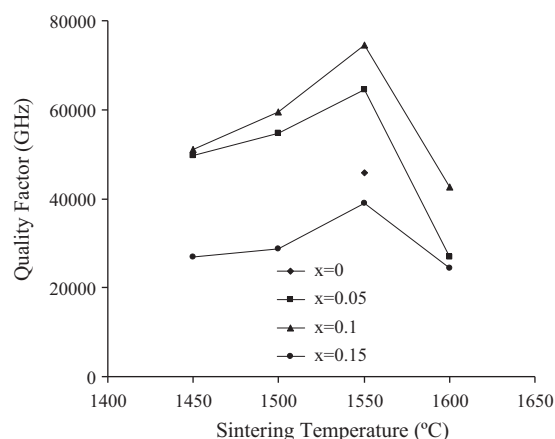
**Fig. 4.** Apparent densities of La(Mg<sub>0.5-x</sub>Ni<sub>x</sub>Sn<sub>0.5</sub>)O<sub>3</sub> ceramics with different degrees of Ni<sup>2+</sup> substitution, following sintering at different temperatures for 4 h.

Fig. 4 shows the apparent densities of La(Mg<sub>0.5-x</sub>Ni<sub>x</sub>Sn<sub>0.5</sub>)O<sub>3</sub> ceramics with different degrees of Ni<sup>2+</sup> substitution, following sintering at 1450–1600 °C for 4 h. The theoretical density of La(Mg<sub>0.5</sub>Sn<sub>0.5</sub>)O<sub>3</sub> ceramic is 6.63 g/cm<sup>3</sup>. The apparent density of La(Mg<sub>0.5-x</sub>Ni<sub>x</sub>Sn<sub>0.5</sub>)O<sub>3</sub> ceramics that were sintered at 1450–1600 °C for 4 h was highest when sintering was carried out at 1550 °C, beyond which temperature, it decreased. The increase in apparent density may be caused by the decrease in the number of pores, as shown in Fig. 3. The maximum apparent density of La(Mg<sub>0.5-x</sub>Ni<sub>x</sub>Sn<sub>0.5</sub>)O<sub>3</sub> ceramics increased from 6.60 to 6.71 g/cm<sup>3</sup> as  $x$  increased from 0 to 0.15. The increase in apparent density is associated with the fact that the Ni atom has a larger mass than the Mg atom.

Fig. 5 shows the dielectric constants of La(Mg<sub>0.5-x</sub>Ni<sub>x</sub>Sn<sub>0.5</sub>)O<sub>3</sub> ceramics with different degrees of Ni<sup>2+</sup> substitution, following sintering at 1450–1600 °C for 4 h. La(Mg<sub>0.35</sub>Ni<sub>0.15</sub>Sn<sub>0.5</sub>)O<sub>3</sub> ceramics that were sintered at 1550 °C for 4 h had a maximum dielectric constant of 20.24. A high sintering temperature was not necessary for obtaining a high dielectric constant. The decrease in dielectric constant was associated with low apparent densities of the ceramics. A higher density is associated with lower porosity, and, therefore, a higher dielectric constant. The dielectric constant increased from 19.94 to 20.24 as  $x$  increased from 0 to 0.15 when the La(Mg<sub>0.5-x</sub>Ni<sub>x</sub>Sn<sub>0.5</sub>)O<sub>3</sub> ceramics were sintered at 1550 °C for 4 h. This fact might be explained by the molar volume. The dielectric



**Fig. 5.** Dielectric constants of La(Mg<sub>0.5-x</sub>Ni<sub>x</sub>Sn<sub>0.5</sub>)O<sub>3</sub> ceramics with different degrees of Ni<sup>2+</sup> substitution, following sintering at different temperatures for 4 h.



**Fig. 6.**  $Q \times f$  of La(Mg<sub>0.5-x</sub>Ni<sub>x</sub>Sn<sub>0.5</sub>)O<sub>3</sub> ceramics with different degrees of Ni<sup>2+</sup> substitution, following sintering at different temperatures for 4 h.

constant can be calculated using the Clausius–Mossotti equation [22]:

$$\epsilon_r = \frac{3V_m + 8\pi\alpha_D}{3V_m - 4\pi\alpha_D} = \frac{1 + (8\pi/3)(\alpha_D/V_m)}{1 - (4\pi/3)(\alpha_D/V_m)} \quad (3)$$

where  $V_m$  is the molar volume,  $\alpha_D$  is the sum of the ionic polarizations of individual ions. Dielectric constants therefore depend on the ionic polarization and the molar volume. As seen from Eq. (3), a larger ionic polarization or a smaller molar volume, is associated with a larger obtained dielectric constant. The polarizations of Mg<sup>2+</sup> ion and Ni<sup>2+</sup> ion are 1.32 and 1.23 Å<sup>3</sup>, respectively [23,24]. The polarization of Mg<sup>2+</sup> ion is almost the same as that of Ni<sup>2+</sup> ion. However, the Ni<sup>2+</sup> ions with smaller ionic radius occupy Mg<sup>2+</sup> ions, and with smaller molar volume, and, therefore, a higher dielectric constant.

Fig. 6 shows the  $Q \times f$  of the La(Mg<sub>0.5-x</sub>Ni<sub>x</sub>Sn<sub>0.5</sub>)O<sub>3</sub> ceramics with different degrees of Ni<sup>2+</sup> substitution, following sintering at 1450–1600 °C for 4 h. La(Mg<sub>0.4</sub>Ni<sub>0.1</sub>Sn<sub>0.5</sub>)O<sub>3</sub> ceramics that were sintered at 1550 °C for 4 h had the highest  $Q \times f$  of 74,600 GHz. The microwave dielectric loss is affected by many factors, which is composed of intrinsic and extrinsic losses. Intrinsic loss is associated with the vibration modes of the lattice. Extrinsic loss is associated with the density, porosity, second phases, impurities, oxygen vacancies, grain size, and lattice defects [25,26]. Since the  $Q \times f$  of La(Mg<sub>0.4</sub>Ni<sub>0.1</sub>Sn<sub>0.5</sub>)O<sub>3</sub> ceramics was consistent with the variation of the apparent density, it is suggested to be dominated by the apparent density. When the La(Mg<sub>0.5-x</sub>Ni<sub>x</sub>Sn<sub>0.5</sub>)O<sub>3</sub> ceramics were sintered at 1550 °C for 4 h, the  $Q \times f$  increased from 45,900 to 74,600 GHz as  $x$  increased from 0 to 0.1, then decreased from 74,600 to 39,000 GHz as  $x$  increased from 0.1 to 0.15. The increase in  $Q \times f$  as  $x$  increased from 0 to 0.1 and decrease in  $Q \times f$  as  $x$  increased from 0.1 to 0.15 might be explained from grain size. Table 1 shows the grain sizes of La(Mg<sub>0.5</sub>Sn<sub>0.5</sub>)O<sub>3</sub>, La(Mg<sub>0.4</sub>Ni<sub>0.1</sub>Sn<sub>0.5</sub>)O<sub>3</sub>, and La(Mg<sub>0.35</sub>Ni<sub>0.15</sub>Sn<sub>0.5</sub>)O<sub>3</sub> are 0.85, 1.43 and 1.29 μm, respectively. The total number of the grain boundaries decreased as the average grain size increased. Grain boundaries acted as plane defects [27]. Less grain boundaries in La(Mg<sub>0.4</sub>Ni<sub>0.1</sub>Sn<sub>0.5</sub>)O<sub>3</sub> ceramics compared with that of La(Mg<sub>0.5</sub>Sn<sub>0.5</sub>)O<sub>3</sub> and La(Mg<sub>0.35</sub>Ni<sub>0.15</sub>Sn<sub>0.5</sub>)O<sub>3</sub>. Besides density and grain size, the amount of second phase also plays an important role in affecting  $Q \times f$ . The formation of second phase of La<sub>2</sub>Sn<sub>2</sub>O<sub>7</sub> might deteriorate the quality factor of the specimen. Table 1 shows the amount of main phase increased from 89.09% to 91.98% as  $x$  increased from 0 to 0.15, and, therefore, the amount of second phase La<sub>2</sub>Sn<sub>2</sub>O<sub>7</sub> decreased from 10.91% to 8.02%.

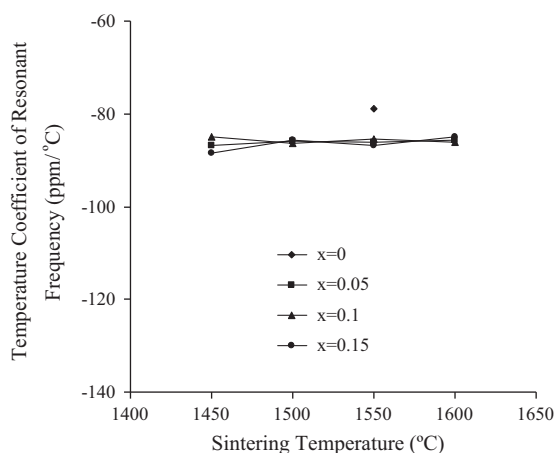


Fig. 7.  $\tau_f$  of  $\text{La}(\text{Mg}_{0.5-x}\text{Ni}_x\text{Sn}_{0.5})\text{O}_3$  ceramics with different degrees of  $\text{Ni}^{2+}$  substitution, following sintering at different temperatures for 4 h.

Fig. 7 shows the temperature coefficient of resonant frequency ( $\tau_f$ ) of  $\text{La}(\text{Mg}_{0.5-x}\text{Ni}_x\text{Sn}_{0.5})\text{O}_3$  ceramics with different degrees of  $\text{Ni}^{2+}$  substitution, following sintering at 1450–1600 °C for 4 h. Generally,  $\tau_f$  is related to the composition, the amount of additive and the second phases that are present in the ceramics. No significant variation in  $\tau_f$  of  $\text{La}(\text{Mg}_{0.5-x}\text{Ni}_x\text{Sn}_{0.5})\text{O}_3$  ceramics with sintering temperature over the entire range of sintering temperatures considered herein was observed. Since the composition of  $\text{La}(\text{Mg}_{0.5-x}\text{Ni}_x\text{Sn}_{0.5})\text{O}_3$  ceramics with a fixed amount of  $\text{Ni}^{2+}$  substitution did not vary with sintering temperature. Although the influence of the degrees of  $\text{Ni}^{2+}$  substitution on the dielectric constant and  $Q \times f$  was observed as described above, no significant variation in  $\tau_f$  was observed. For perovskite ceramic, the  $\tau_f$  is related to the tilting of oxygen octahedron [21]. The tilting of oxygen octahedron is controlled by the tolerance factor of the perovskite ceramic. Since the variation of tolerance factor in  $\text{La}(\text{Mg}_{0.5-x}\text{Ni}_x\text{Sn}_{0.5})\text{O}_3$  series was slight, the effect of tolerance factor on the  $\tau_f$  can be ignored in this study. A  $\tau_f$  of  $-85 \text{ ppm/}^\circ\text{C}$  was measured for  $\text{La}(\text{Mg}_{0.4}\text{Ni}_{0.1}\text{Sn}_{0.5})\text{O}_3$  ceramics that were sintered at 1550 °C for 4 h.

#### 4. Conclusions

The effects of the degree of  $\text{Ni}^{2+}$  substitution and sintering temperature on the microwave dielectric properties of

$\text{La}(\text{Mg}_{0.5-x}\text{Ni}_x\text{Sn}_{0.5})\text{O}_3$  ceramics were studied. The microwave dielectric properties of  $\text{La}(\text{Mg}_{0.5-x}\text{Ni}_x\text{Sn}_{0.5})\text{O}_3$  ceramics were improved by substituting  $\text{Mg}^{2+}$  ions for  $\text{Ni}^{2+}$  ions. The X-ray diffraction peaks of  $\text{La}(\text{Mg}_{0.4}\text{Ni}_{0.1}\text{Sn}_{0.5})\text{O}_3$  ceramics did not vary significantly with sintering temperature. The diffraction peaks of  $\text{La}(\text{Mg}_{0.5-x}\text{Ni}_x\text{Sn}_{0.5})\text{O}_3$  ceramics shifted to higher angles and the amount of second phase  $\text{La}_2\text{Sn}_2\text{O}_7$  decreased as  $x$  increased.  $\text{La}(\text{Mg}_{0.4}\text{Ni}_{0.1}\text{Sn}_{0.5})\text{O}_3$  ceramics that were sintered at 1550 °C for 4 h had an apparent density of  $6.71 \text{ g/cm}^3$ , a dielectric constant of 20.19, a  $Q \times f$  of 74,600 GHz, and a temperature coefficient of resonant frequency ( $\tau_f$ ) of  $-85 \text{ ppm/}^\circ\text{C}$ . The dielectric constant of  $\text{La}(\text{Mg}_{0.5-x}\text{Ni}_x\text{Sn}_{0.5})\text{O}_3$  ceramics was affected by the density and ionic polarization. The  $Q \times f$  of  $\text{La}(\text{Mg}_{0.5-x}\text{Ni}_x\text{Sn}_{0.5})\text{O}_3$  ceramics depended on the density, grain size, and amount of second phase.

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